



# Virtual Formulation Laboratory

for prediction and optimisation of  
manufacturability  
of advanced solids based formulations

Powder Flow 2018: Cohesive Powder Flow

organised by

Formulation Science and Technology group (FSTG) of the Royal Society of Chemistry

12 April 2018 Burlington House, London



EPSRC

Engineering and Physical Sciences  
Research Council

# Academic Collaborators

- Csaba Sinka, Ruslan Davidchack, Ben Edmans, Nicodemo Di Pasquale  
University of Leicester
- Mojtaba Ghadiri, Xiaodong Jia, Mehrdad Pasha  
University of Leeds
- Mike Bradley, Rob Berry, Pablo Garcia Trinanes, Baldeep Kaur  
University of Greenwich
- Jerry Heng, Vikram Karde  
Imperial College



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for Bulk Solids Handling Technology

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# Industrial Partners

- Centre for Process Innovation (CPI)
- Procter & Gamble
- GlaxoSmithKline
- AstraZeneca
- Nestle
- KP Snacks
- Chemours
- Malvern Instrument
- Brookfield
- Britest
- Process Systems Enterprise (PSE)
- Griffiths Food
- Freeman Technology
- DEM Solutions



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# VFL: 4 Processes/ 4 Problems



Molecule level information

Particle level information

Bulk level information



Prediction of flow/  
arching, flooding

Prediction of mixing/  
segregation

Prediction of storage/  
caking

Prediction of compact/  
breakage

Hierarchical input structure

Manufacturability indicators (MI)



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# Surface Free Energy Predictions



Dr Nicodemo Di Pasquale and Prof. Ruslan Davidchack

- Prediction of Adhesive Interactions by Molecular dynamics (MD), using Cleaving Method
- Comparison of results from MD simulation with FD-IGC experimental work at ICL

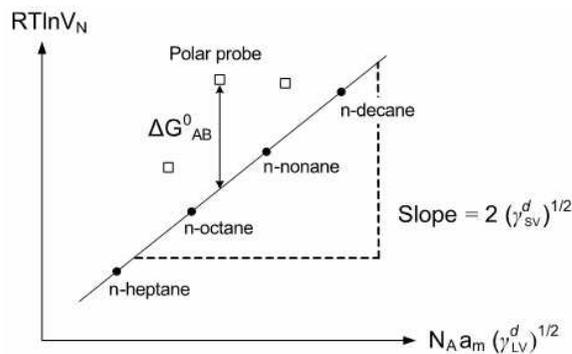
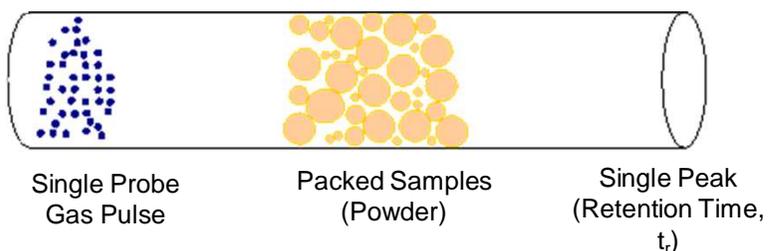


# Surface Energy Characterisation using Inverse Gas Chromatography (FD-IGC)

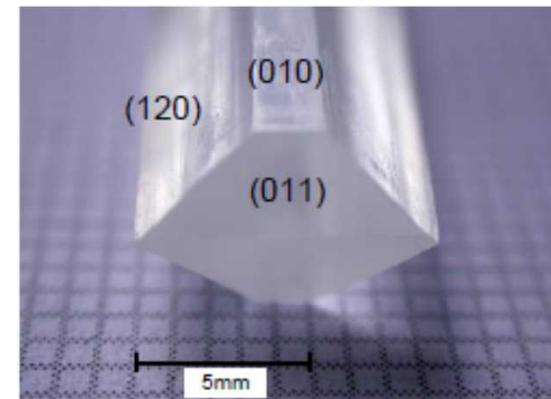
## Dr Vikram Karde and Dr Jerry Heng



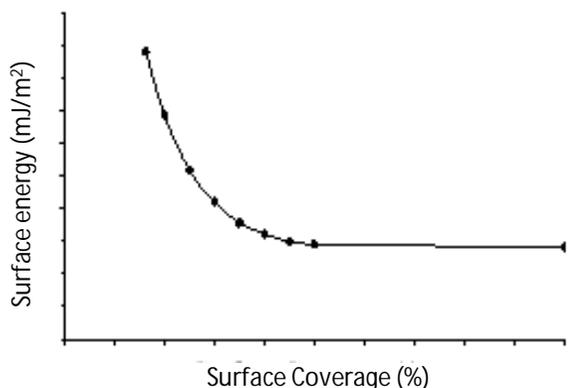
Surface energy determination using IGC



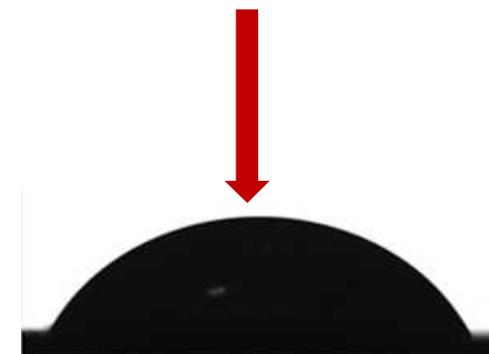
Anisotropy in crystalline solids (Heterogeneous surfaces)



Surface energy heterogeneity using Finite Dilution IGC (FD-IGC)



Surface energy heterogeneity profile



Facet specific surface energy using Contact angle



# Flowability, Mixing, Segregation

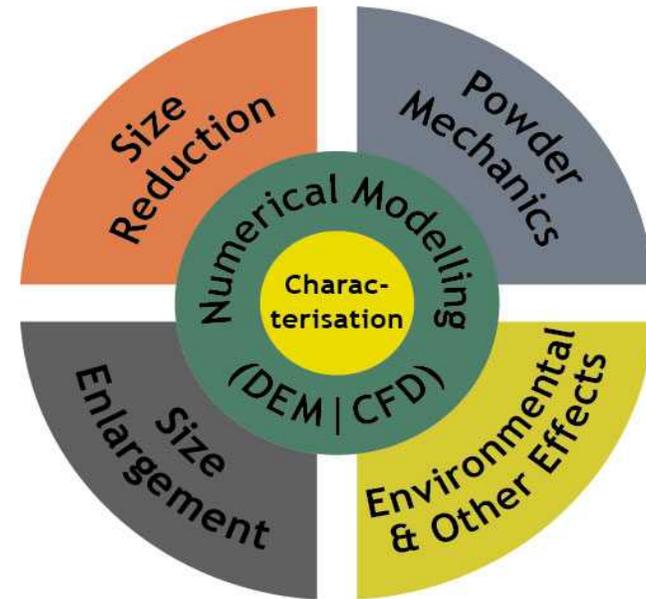
Dr Mehrdad Pasha, Dr Xiaodong Jia and Prof. Mojtaba Ghadiri

Single particle characterisation

Particle assembly behaviour prediction by DEM

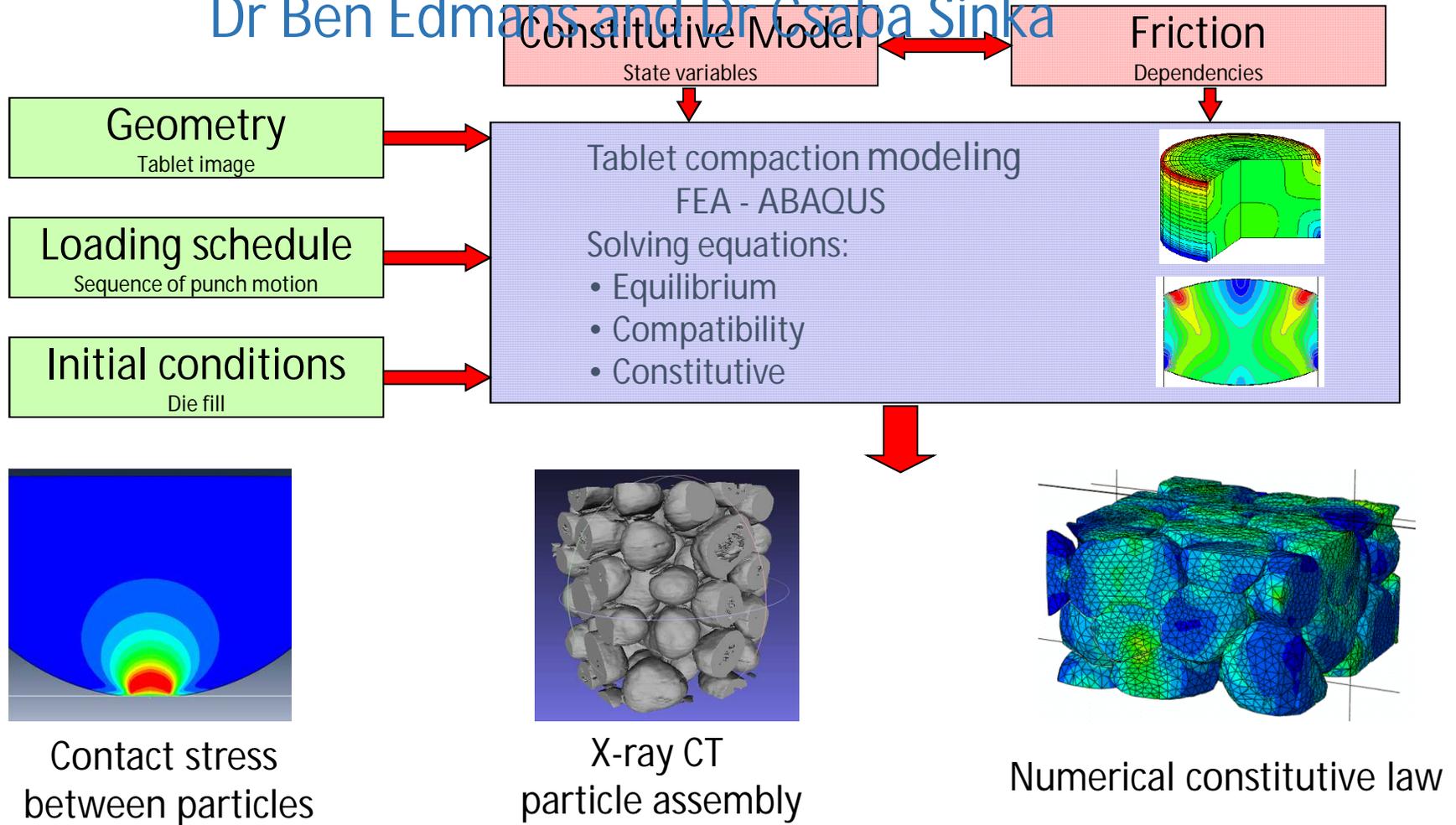
Experimental validation

VFL Toolkit development in a collaborative way



# Modelling Powder Compaction

Dr Ben Edmans and Dr Csaba Sinka



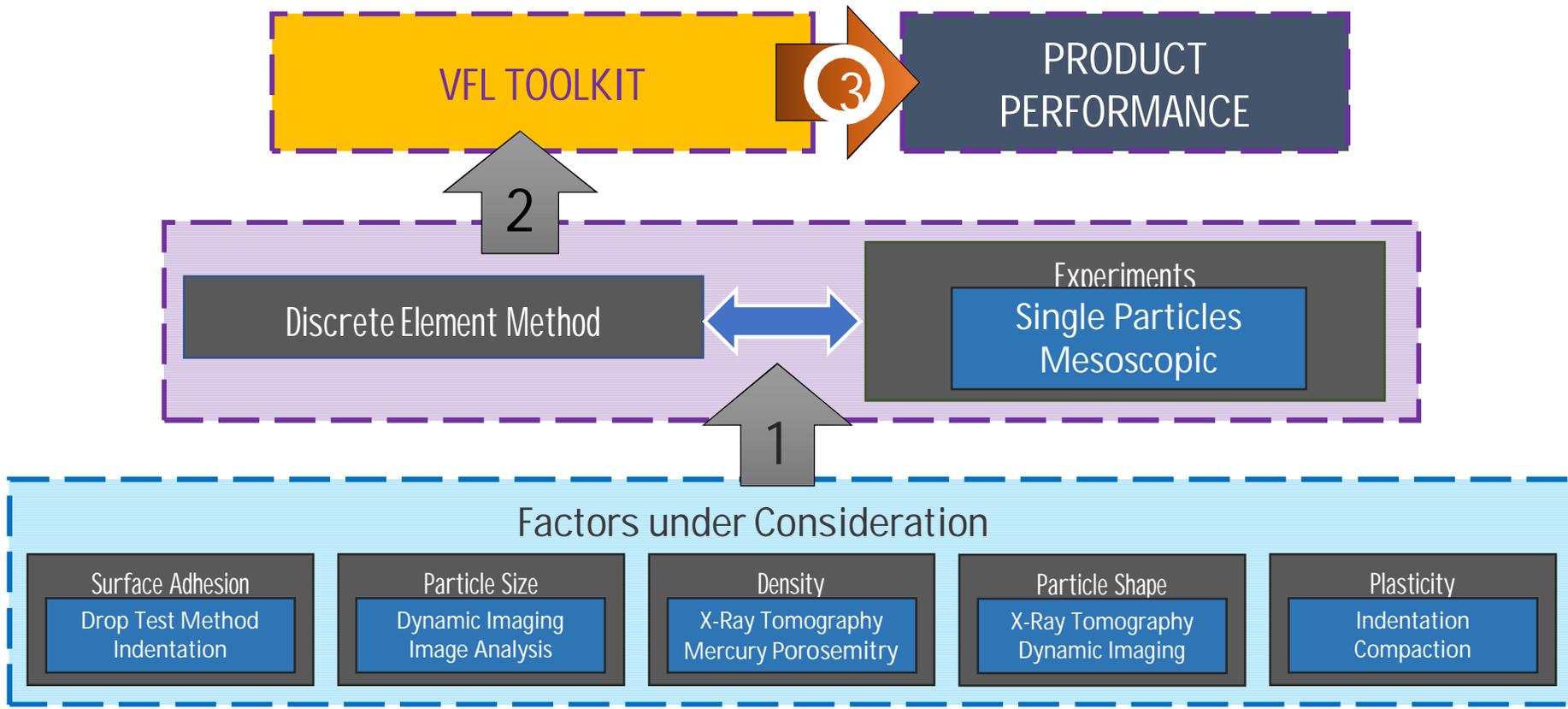
# Particle and Bulk Scale Measurements

Dr Pablo Garcia Trinanes, Dr Rob Berry and Prof. Michael Bradley

- **Particle size and shape measurement**
  - G3 morphologi – shape/ size
  - Air-swept sieve – size
  - Pycnometer – material density
- **Bulk flow properties**
  - Brookfield (PFT) - freeman for high stress tests? – flow function, friction, bulk density (voidage)
  - Uniaxial compaction test – for high stress tests
- **Segregation properties**
  - Free surface (rolling segregation) for coarse particles > approx. 100 mm
  - Air induced (elutriation) for separation of fines (sub 50 mm) from wider distribution
- **Caking properties**
  - Capability for measuring cake strengths driven by:
    - moisture migration, chemical reaction or plastic flow mechanisms in storage

# Work Plan of Leeds

Flowability | Segregation | Mixing



# Material Characterisation

## Surface Adhesion

### Method

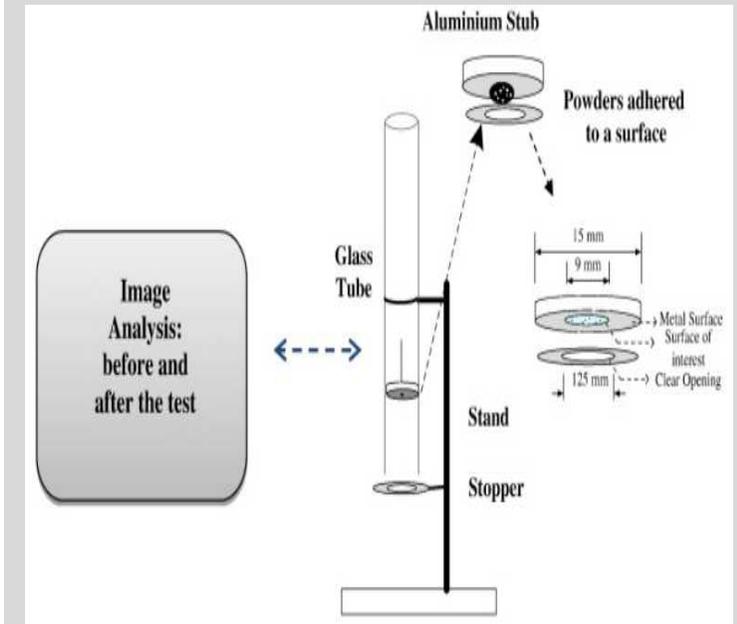
- The powder will be dispersed into a flat target (material of interest) using Malvern G3 Morphologi disperser.
- The target will then be dropped from a range of heights until a satisfactory detachment of particles is observed by image analysis.
- Two images, before and after the drop, are taken by SEM to assess the detached and attached particles on the surface of the target

### Calculations

$$\frac{F_d}{F_{ad}} = \frac{mv}{\frac{3}{2}\pi R\Gamma \Delta t} = L$$

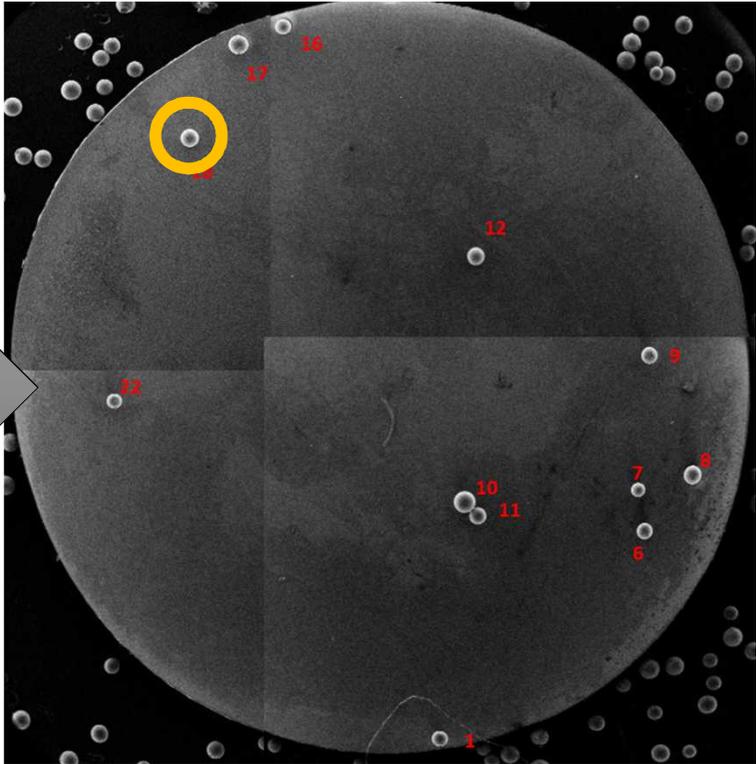
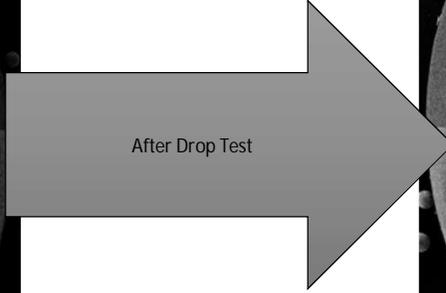
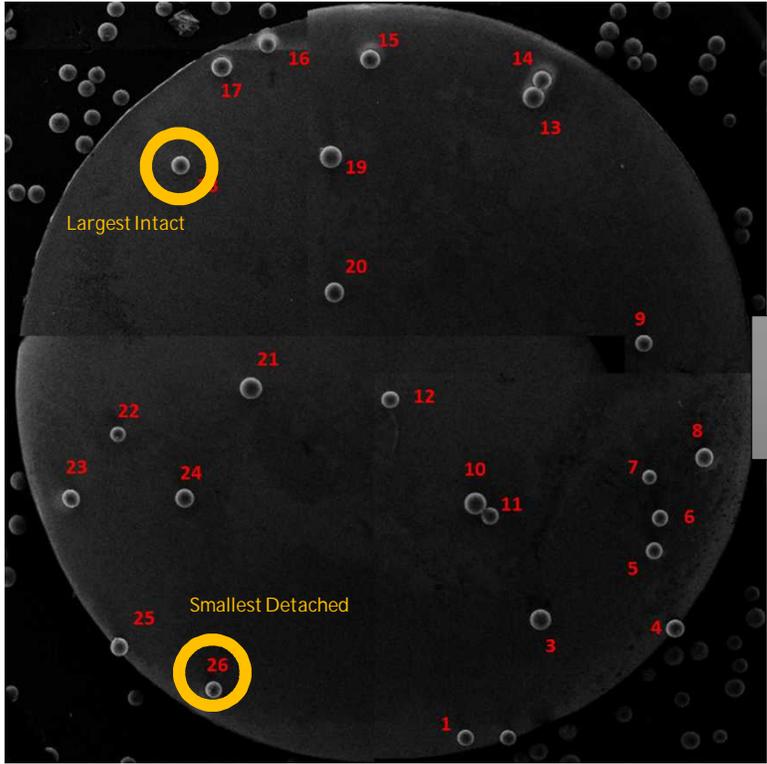
$$R = \frac{\text{smallest detached particle} + \text{largest attached particle}}{2}$$

### Schematic



# Material Characterisation

## Surface Adhesion



# Measurement of Surface Energy

Leeds Drop Test Method: **Results**

Materials: Glass Ballotini (90 – 200  $\mu\text{m}$ ), Glass Plate (5 mm in diameter), Steel Plate (5 mm in diameter)

Interactions:

- 1) Silanised Glass Ballotini vs Silanised Glass Ballotini/Plate (SGB-SGB)
- 2) Silanised Glass Ballotini vs Non-Silanised Glass Ballotini/Plate (SGB-NSGB)
- 3) Silanised Glass Ballotini vs. Steel Plate (SGB-SP)

## Drop Test Results

SGB – SGB

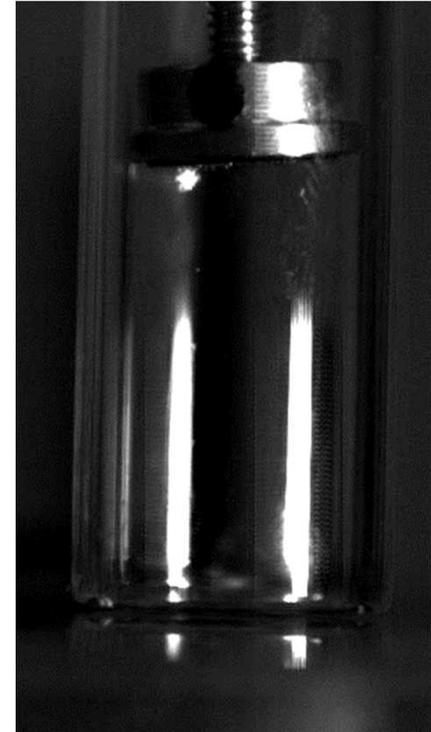
$$G_{SGB-SGB} = 27.4 \text{ } \mu\text{mJ/m}^2$$

SGB – NSGB

$$G_{SGB-NSGB} = 20.6 \text{ } \mu\text{mJ/m}^2$$

SGB – SP

$$G_{SGB-SP} = 24.4 \text{ } \mu\text{mJ/m}^2$$

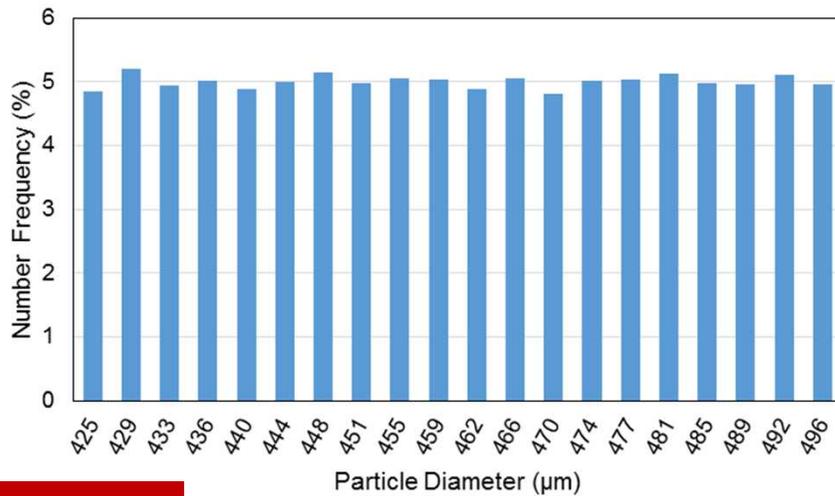


# Flowability by FT4

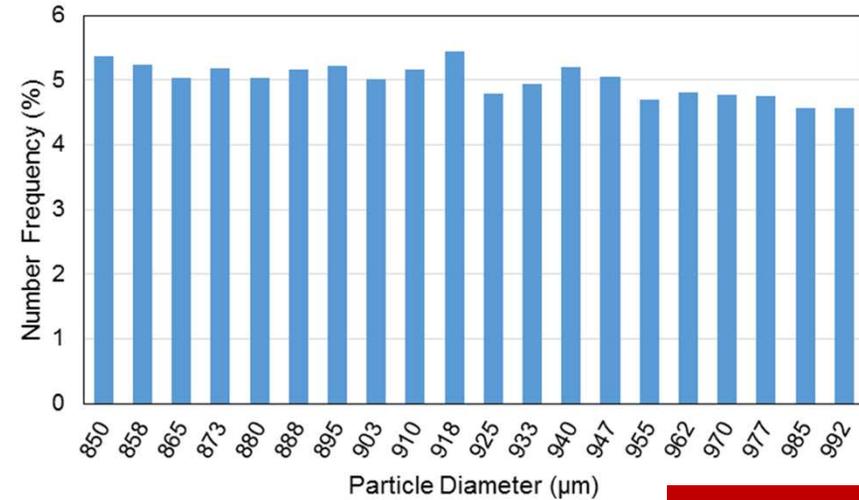
Effect of Particle Size: Material

q Two size classes of glass ballotini were chosen:

- ✓ 425 – 500  $\mu\text{m}$  (on the left)
- ✓ 850 – 1000  $\mu\text{m}$  (on the right)



425 – 500  $\mu\text{m}$



850 – 1000  $\mu\text{m}$

# Flowability

Effect of Particle Size: Material

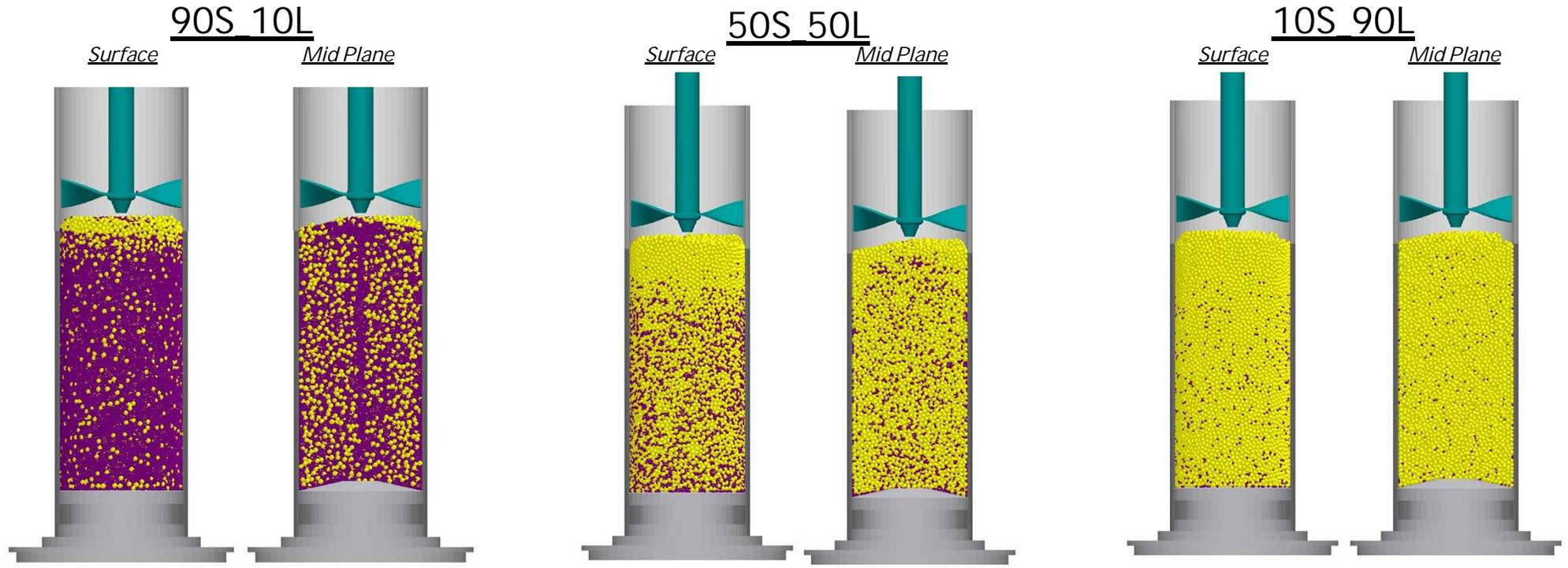


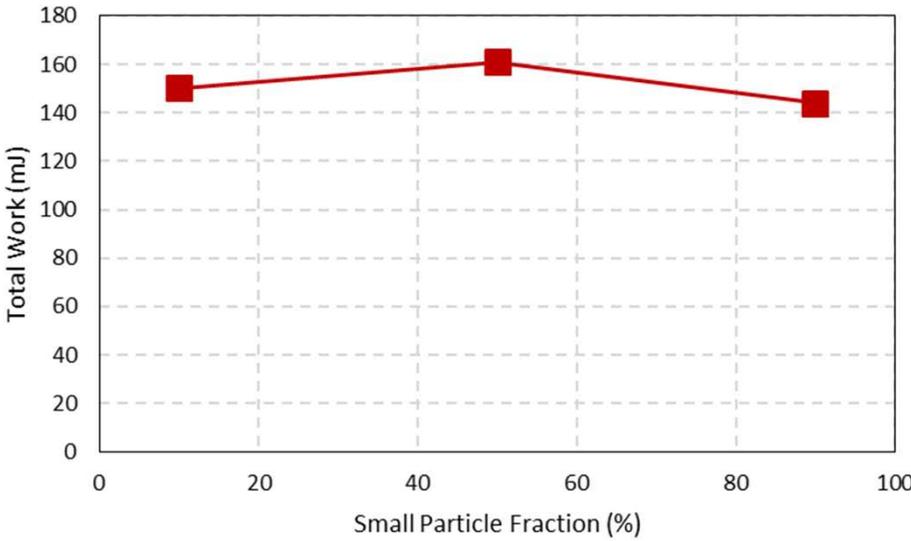
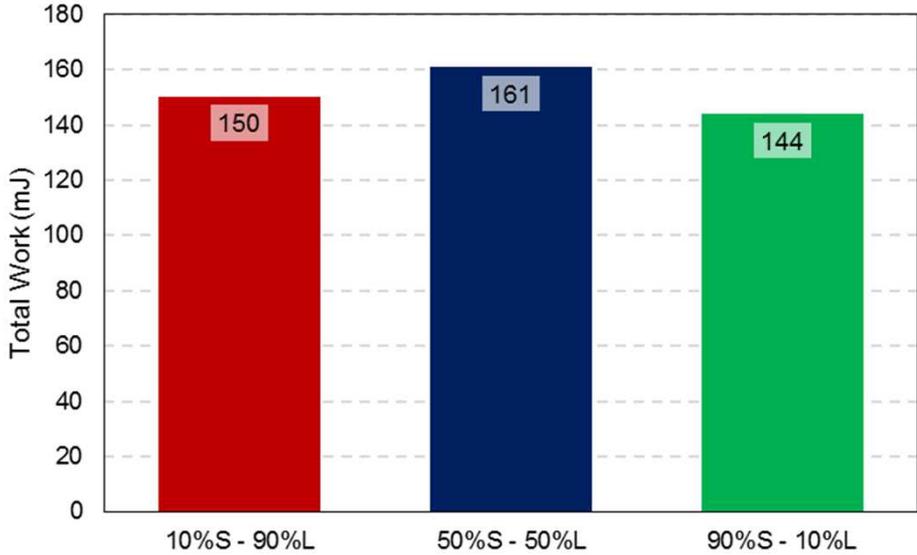
Three mixtures are considered as follow based on number ratio

q 10% (425 – 500 μm) & 90% (850 – 1000 μm) referred to 10S\_90L

q 50% (425 – 500 μm) & 50% (850 – 1000 μm) referred to 50S\_50L

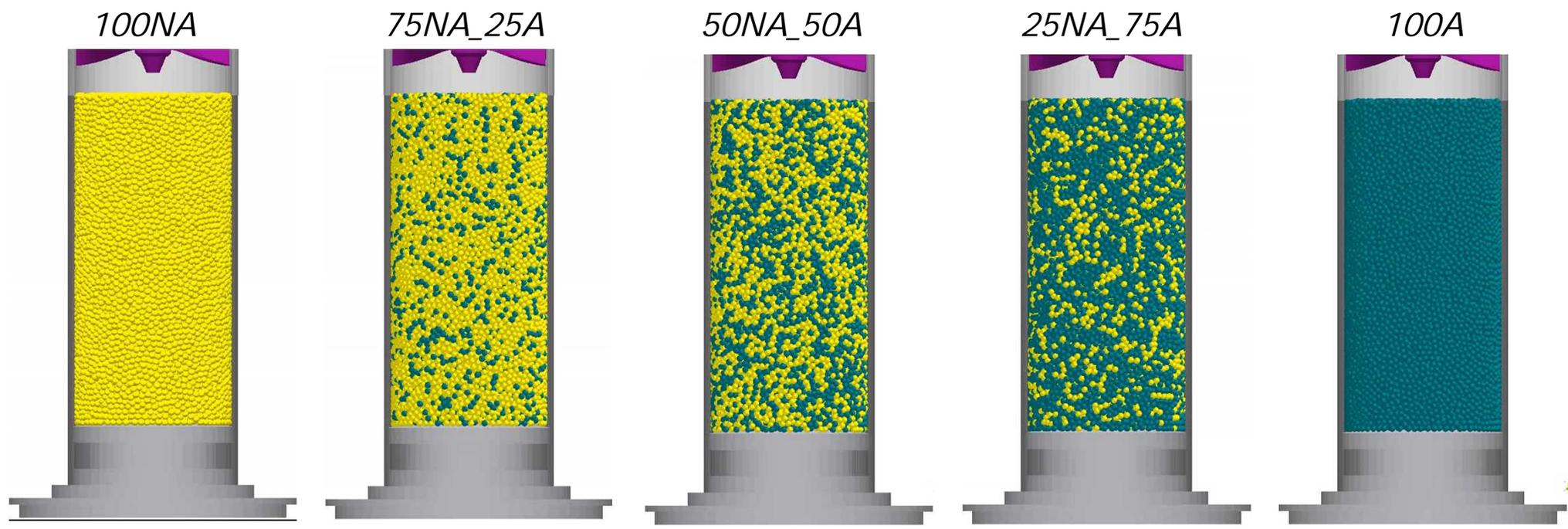
q 90% (425 – 500 μm) & 10% (850 – 1000 μm) referred to 90S\_10L





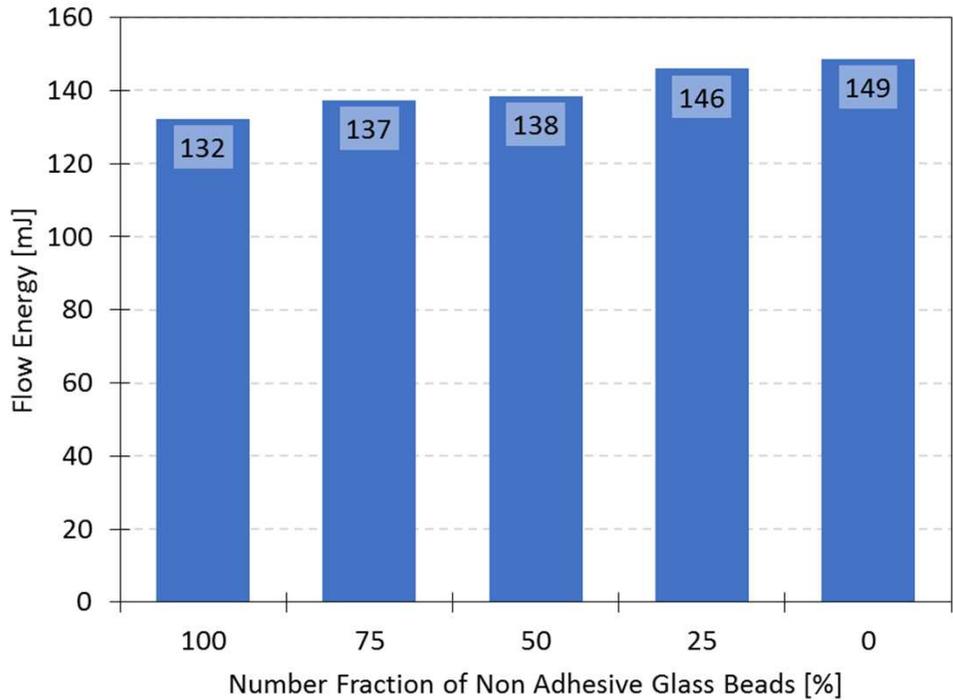
# Flowability

Effect of Particle Adhesion: **Downward Test Results**



# Flowability

Effect of Particle Adhesion: **Downward Test Results**



Number Fraction NSGB [%]	Number Fraction SGB [%]	Flow Energy [mJ]
100	0	132.3
75	25	137.4
50	50	138.5
25	75	145.9
0	100	148.7

# Manufacturability Index for Powder Flow

The Approach of Capece *et al.*\*

## Flow Function and Granular Bond Number For Multi-Component Powder Bed

$$ff_{c,mix} = a \left( Bo_{g,mix} \right)^{-b}$$

$$Bo_{g,Mix} = \frac{\alpha \prod_{i=1}^N \dot{\alpha} \prod_{j=1}^N \frac{w_{ij}}{Bo_{g,ij}}}{\dot{\alpha} \prod_{i=1}^N \dot{\alpha} \prod_{j=1}^N \frac{w_{ij}}{Bo_{g,ij}}}$$

$w_{ij}$  is the interaction weighting factor

where  $\alpha$  and  $\beta$  are the fitting parameters

$$Bo_{g,ij} = \frac{F_{ad,ij}}{W_{ij}}$$

$$W_{ij} = \frac{2W_i W_j}{W_i + W_j}$$

$\alpha$  is the flow function at the cohesive-non-cohesive boundary ( $Bo_{g,mix}=1$ )

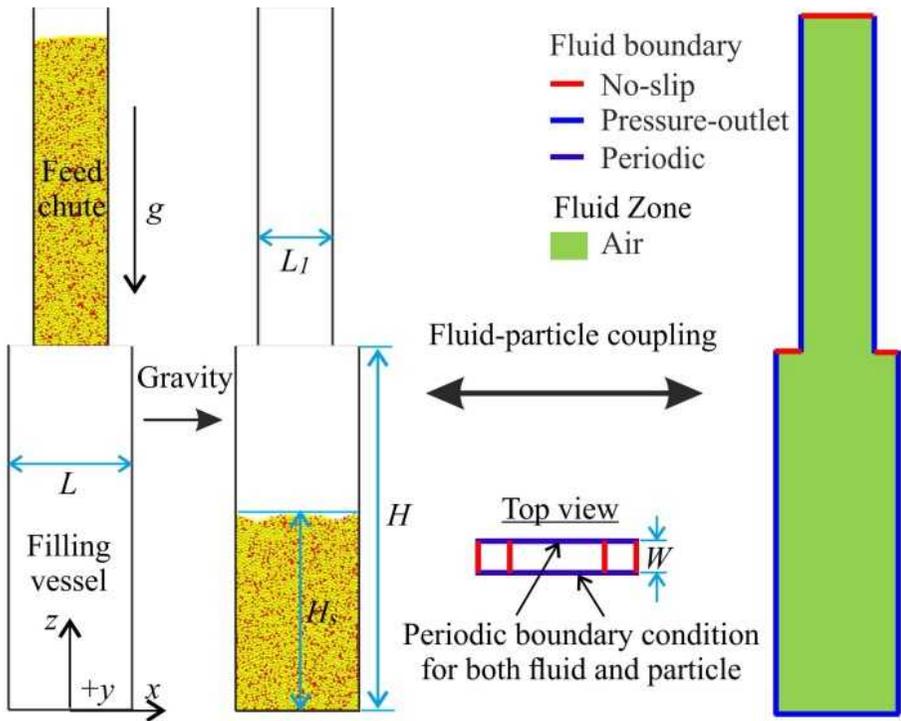
$$w_{ij} = f_{SA,i} f_{SA,j}$$

$f_{SA}$  is the fractional surface area that gives the likelihood that the two material ( $i$  and  $j$ ) come into contact

\*Capece *et al.* (2015), Powder Technology 286 561–571

# Elutriation Segregation

(Dr W. Nan)



Aspects under investigation:

- ∅ Effect of the depth of filling vessel
- ∅ Effect of inlet ratio
- ∅ Effect of size ratio and density ratio



# Simulation Parameters



Parameters	Basic Value	Value range
Geometry		
Length (mm), L	10	-
Depth (mm), H	60	30-180
Width (mm), W	2	-
Inlet ratio, IR	0.6	0.4-1.0
Gas (air)		
Density (kg/m <sup>3</sup> ), $\rho_f$	1.2	-
Viscosity (Pa·s), $\mu_f$	$1.8 \times 10^{-5}$	-
Particle		
Diameter (mm), $d_p$		
Fine particle, $d_{p,f}$	0.1375	-
Coarse particle, $d_{p,c}$	0.275	0.275, 0.55
Density (kg/m <sup>3</sup> ), $\rho$		
Fine particle, $d_{p,f}$	1300	-
Coarse particle, $d_{p,c}$	1300	1300, 7800
Volume fraction of fine particle, $x_f$	0.1	-
Poisson's ratio, $\nu$	0.3	-
Shear modulus (MPa), G	10	-
Restitution coefficient, e	0.42	-
Friction coefficient, $\mu$	0.5	-

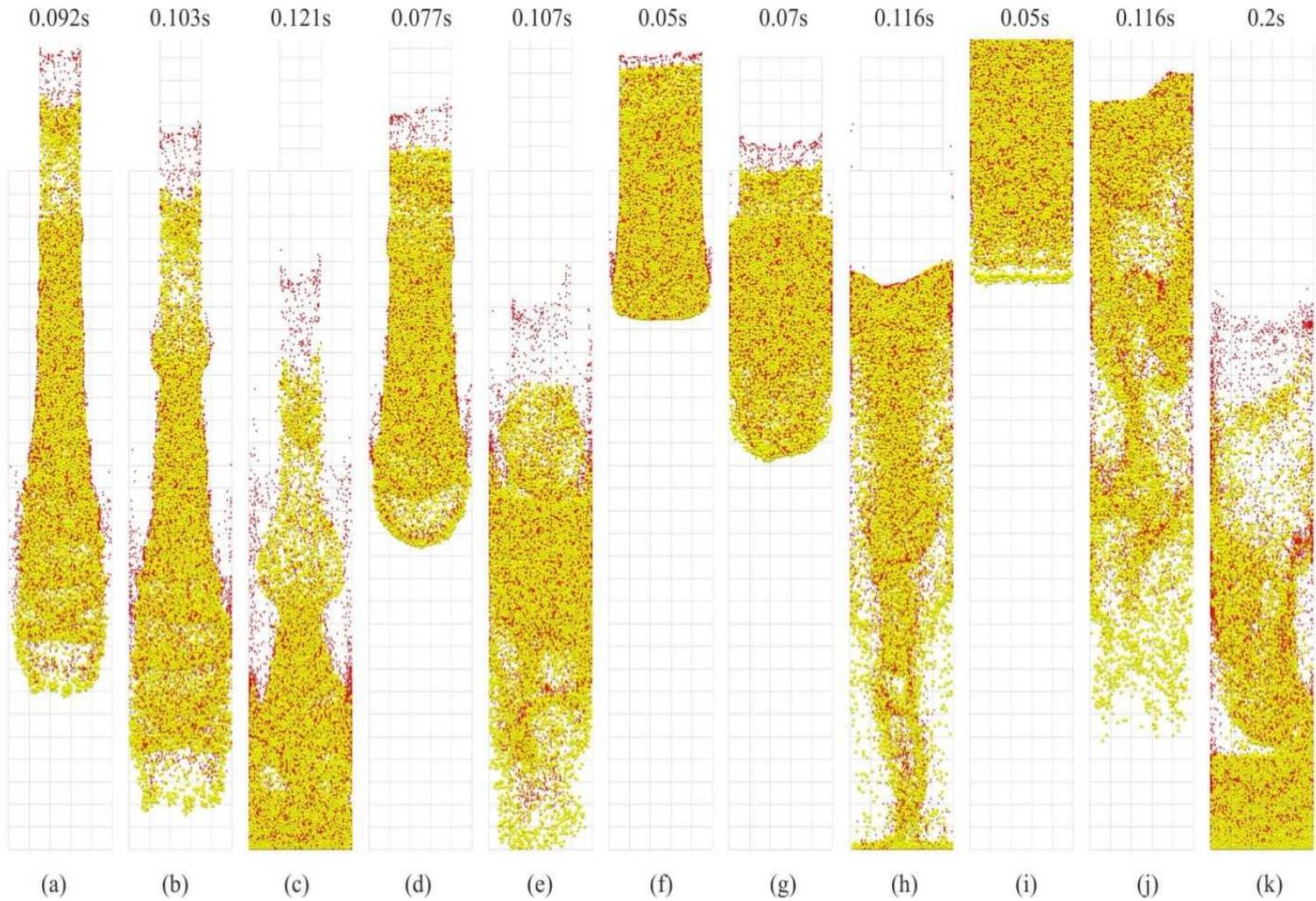




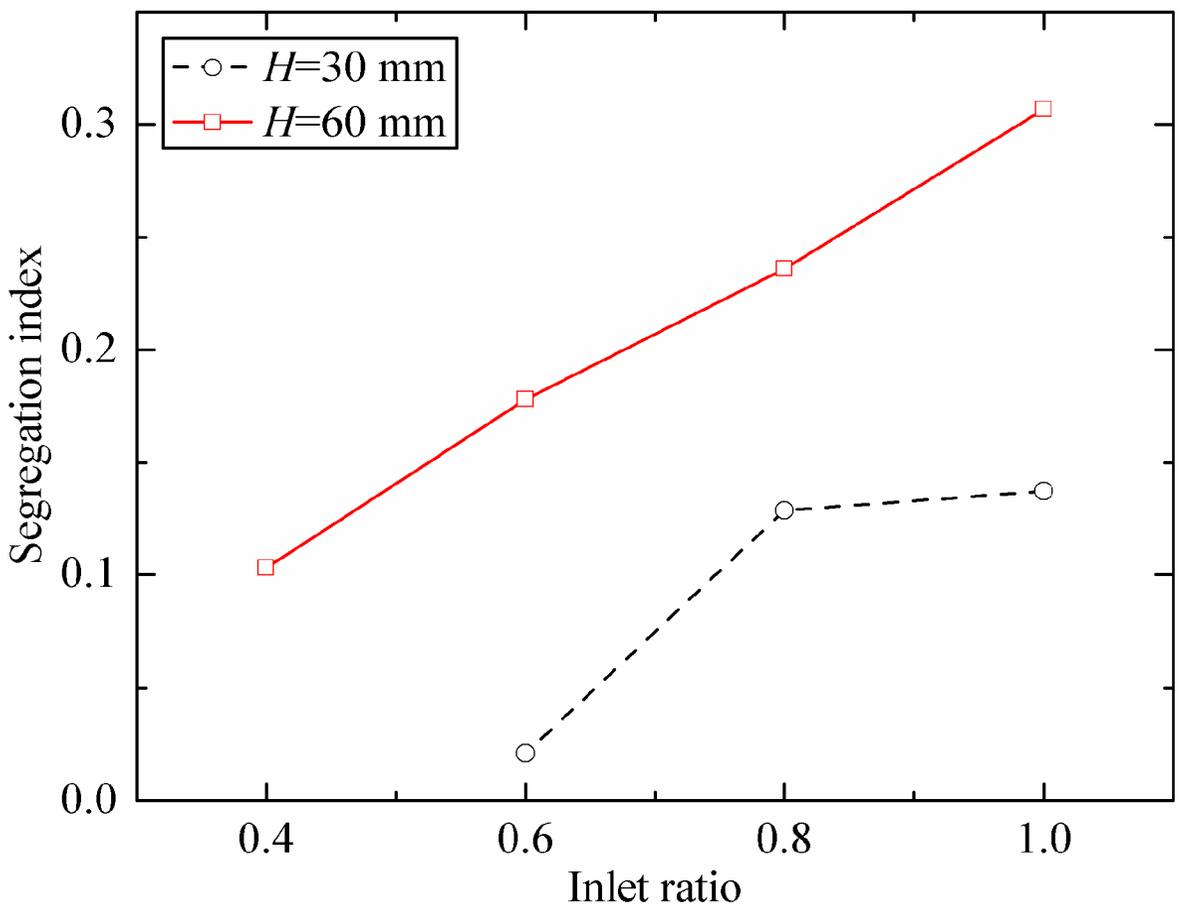
# Effect of Inlet Ratio



IR=0.4 (a-c), IR=0.6 (d-e), IR=0.8 (f-h) and IR=1.0 (j-k)

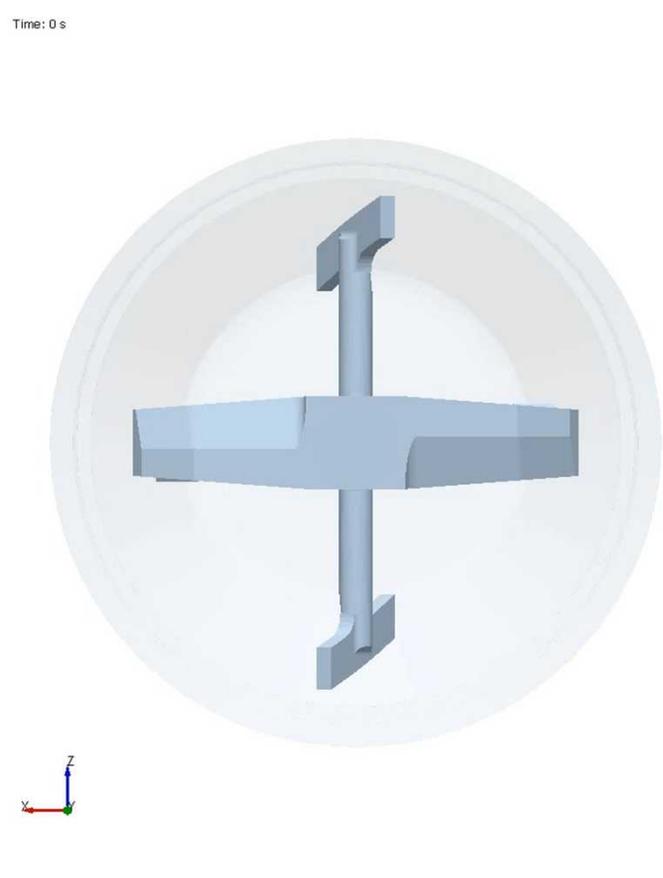


# Effect of the inlet ratio on the vertical segregation index



$$SI = \frac{\sigma}{\bar{x}}$$

# Mixing and Segregation



# Concluding remarks



- develop the science base for understanding of particle surfaces, structures and bulk behaviour to address physical, chemical and mechanical properties and behaviour during processing and storage
- develop formulation science to link molecule to manufacturability (through experimental characterisation and numerical modelling)
- establish methodologies to formulate new materials through developing functional relationships, considering the limits and uncertainties
- Develop a software tool for prediction and optimisation of manufacturability and stability of advanced solids-based formulations





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